

# ON A SOLUTION TO THE EQUATIONS OF MAGNETO-GASDYNAMICS

(K RESHENIUI URAVNENII MAGNITNOI GAZODINAMIKI)

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An investigation of strong and weak discontinuities in magneto-hydrodynamics is contained in a series of papers and books (see, for instance, [1-4]). In the following, the equations of planar flow in a magnetic field parallel to the velocity field are transformed under certain initial restraints to a linear equation of the Chaplygin type [5]. We will apply the result to a problem in which there are no strong discontinuities.

The equations of the steady motion of a gas with infinite conductivity in a magnetic field have the following form:

$$\operatorname{div} \mathbf{H} = 0, \quad \operatorname{rot} (\mathbf{W} \times \mathbf{H}) = 0, \quad \operatorname{div} \rho \mathbf{W} = 0, \quad (\mathbf{W} \cdot \nabla) \mathbf{W} = -\frac{\operatorname{grad} p}{\rho} - \frac{1}{4\pi\rho} \mathbf{H} \times \operatorname{rot} \mathbf{H} \quad (1)$$

where  $\mathbf{H}$  is the magnetic field strength,  $p$ ,  $\rho$  and  $\mathbf{W}$  are respectively the pressure, density and vector velocity of the flow. If the flow is planar and the vector  $\mathbf{H}$  lies in the plane of the flow, it follows from the second of Equations (1) that  $\mathbf{W} \times \mathbf{H} = \text{const}$ . If  $\mathbf{W} \parallel \mathbf{H}$  at one point, then  $\mathbf{W} \parallel \mathbf{H}$  throughout the flow field. One can write

$$\mathbf{H} = k(x, y) \rho \mathbf{W} \quad (2)$$

where  $k(x, y)$  is the coefficient of proportionality.

From the first and third equations of the system (1) we conclude that  $k(x, y) = \text{const}$  along a streamline. The vector  $\mathbf{H} \times \operatorname{rot} \mathbf{H}$  is perpendicular to the streamline. Therefore, the Bernoulli formula

$$w dw + \frac{dp}{\rho} = 0 \quad (3)$$

is correct along streamlines.

Let us assume  $p = p(\rho)$  and let formula (3) be correct in any direction in the region of flow. We will also consider subsequently that  $k = \text{const}$  throughout the flow, which obtains in particular for the undisturbed

parallel flow at infinity. On the basis of (3) we have

$$p = p(w), \quad p = - \int \rho(w) w dw \quad (4)$$

from which there follows

$$\frac{1}{\rho} \text{grad } p = - \text{grad } \frac{w^2}{2} \quad (5)$$

On the other hand,  $(W \cdot \nabla) W = \text{rot } W \times W + \text{grad } \frac{1}{2} W^2$ . Therefore, the last equation of the system (1) reduces to the form

$$\text{rot } W \times W = - \frac{1}{4\pi\rho} H \times \text{rot } H \quad (6)$$

Projecting Equation (6) on to the coordinate axes  $x, y$  and taking formula (2) into account, we obtain

$$\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = \frac{k^2}{4\pi} \left( \frac{\partial \rho v}{\partial x} - \frac{\partial \rho u}{\partial y} \right), \quad \text{и} \quad \frac{\partial v^*}{\partial x} - \frac{\partial u^*}{\partial y} = 0 \quad (7)$$

where

$$u^* = w^* \cos \theta, \quad v^* = w^* \sin \theta, \quad w^* = w \left( 1 - \frac{k^2}{4\pi} \rho \right) \quad (8)$$

and  $\theta$  is the angle of the velocity vector with the abscissa.

The existence of a stream function  $\psi(x, y)$

$$\frac{\partial \psi}{\partial x} = -v\rho(w) = -v^*\rho^*(w^*), \quad \frac{\partial \psi}{\partial y} = u\rho(w) = u^*\rho^*(w^*) \quad \left( \rho^* = \frac{\rho}{1 - k^2\rho/4\pi} \right) \quad (9)$$

follows from the continuity equation.

Equation (7) permits a fictitious potential  $\phi$  to be introduced in accordance with the formula

$$\frac{\partial \phi}{\partial x} = u^*, \quad \frac{\partial \phi}{\partial y} = v^* \quad (10)$$

As is well-known from the equations of total differential expressions

$$dx = \frac{\cos \theta}{w^*} d\phi - \frac{\sin \theta}{\rho^* w^*} d\psi, \quad dy = \frac{\sin \theta}{w^*} d\phi + \frac{\cos \theta}{\rho^* w^*} d\psi \quad (11)$$

one can derive the following system of equations for the unknown function  $\phi$  and  $\psi$ :

$$\frac{\partial \phi}{\partial \theta} = \frac{w^*}{\rho^*} \frac{\partial \psi}{\partial w^*}, \quad \frac{\partial \phi}{\partial w^*} = w^* \frac{d}{dw^*} \left( \frac{1}{\rho^* w^*} \right) \frac{\partial \psi}{\partial \theta} \quad (12)$$

The system (12) has the canonical form

$$\frac{\partial \phi}{\partial \theta} = \sqrt{K} \frac{\partial \psi}{\partial s}, \quad \frac{\partial \phi}{\partial s} = -\sqrt{K} \frac{\partial \psi}{\partial \theta} \quad (13)$$

where the functions of the velocity  $\sqrt{K}$  and  $s$  are related to  $w^*$  and  $\rho^*$  in

accordance with (6) by the formulas

$$\frac{dQ}{ds} = -\sqrt{K}P, \quad Q = \sqrt{K} \frac{dP}{ds} \quad (P = w^{\gamma-1}, Q = (\rho^* w^*)^{-1}) \quad (14)$$

hence

$$ds = \left( \frac{P'(w^*) Q'(w^*)}{P(w^*) Q(w^*)} \right)^{1/2} dw^*, \quad \sqrt{K} = \left( \frac{Q(w^*) Q'(w^*)}{P(w^*) P'(w^*)} \right)^{1/2} \quad (15)$$

Substituting expressions for the functions  $P(w^*)$  and  $Q(w^*)$  into (15) and taking into consideration formulas (8) and (9) and the formula for determining the velocity of sound

$$a^2 = \frac{dp}{d\rho} = -\frac{wp(w)}{\rho'(w)} \quad (16)$$

we obtain

$$\sqrt{K} = \frac{1}{\rho} \left( \frac{(1-M^2)(1-m\rho)^3}{1-m\rho(1-M^2)} \right)^{1/2}, \quad ds = \pm \left( \frac{(1-M^2)[1-m\rho(1-M^2)]}{1-m\rho} \right)^{1/2} \frac{dw}{w} \quad (m = k^2/4\pi)$$

where  $M$  is the Mach number. The negative sign in (17) is taken for the interval of variation of  $w$  in which  $dw^*/ds < 0$ . For imaginary values of  $s$  and  $\sqrt{K}$  we have the hyperbolic system of equations

$$\frac{\partial\varphi}{\partial\theta} = \sqrt{\chi} \frac{\partial\psi}{\partial\sigma}, \quad \frac{\partial\varphi}{\partial\sigma} = \sqrt{\chi} \frac{\partial\psi}{\partial\theta} \quad (\sigma = -is, \sqrt{\chi} = -i\sqrt{K}) \quad (18)$$

In the case  $p = \text{const } \rho^\kappa$ , where  $\kappa$  is the ratio of specific heat coefficients, formulas (17) and (21) take the form

$$\begin{aligned} \sqrt{K} &= \left( \frac{(1-\lambda^2)[1-k_1(1-\lambda^2/h^2)^\gamma]^\beta}{(1-\lambda^2/h^2)^{h^2}[1-k_1(1-\lambda^2/h^2)^\gamma(1-M^2)]} \right)^{1/2} \\ ds &= \pm \left( \frac{(1-\lambda^2)[1-k_1(1-\lambda^2/h^2)^\gamma(1-M^2)]}{(1-\lambda^2/h^2)[1-k_1(1-\lambda^2/h^2)^\gamma]} \right)^{1/2} \frac{d\lambda}{\lambda} \\ \left( k_1 = \frac{k^2}{4\pi} \left( \frac{x+1}{2x} a_*^2 \right)^\gamma, h^2 = \frac{x+1}{x-1}, \gamma = \frac{1}{x-1}, x \neq 1 \right) \end{aligned} \quad (19)$$

where  $\lambda$  is the magnitude of the relative velocity and  $a_*$  is the critical velocity of sound. If  $k_1 < 1$ , the system (13) is correct for  $\lambda < 1$  and the system (18) is correct for  $\lambda > 1$ . The case  $k_1 > 1$  is of greater interest. Then the quantities

$$1 - k_1(1-M^2)(1-\lambda^2/h^2)^\gamma, \quad 1 - k_1(1-\lambda^2/h^2)^\gamma$$

which are negative in the neighborhood of  $\lambda = 0$  vanish respectively for  $\lambda_1 < 1$  and  $\lambda_2 = h(1 - k_1^{1-\kappa})$ , where  $\lambda_2 > \lambda_1$ . In the interval of velocity variation  $0 < \lambda < \lambda_1$  we have for every  $\lambda_2$  the elliptic system of equations (13). If  $\lambda_2 < 1$ , we have for the subsonic interval  $\lambda_1 < \lambda < \lambda_2$  the hyperbolic system of equations (18), and subsequently for the interval

$\lambda_2 < \lambda < 1$  the elliptic system of equations (13), and finally for  $\lambda > 1$  again the system (18). If  $\lambda_2 > 1$ , the system (18) is correct for the intervals  $\lambda_1 < \lambda < 1$  and  $\lambda_2 < \lambda < h$ , and the elliptic system of equations (13) for the supersonic interval  $1 < \lambda < \lambda_2$ . If

$$\lambda_2 = 1, \text{ или } k_1 = \left(\frac{h}{h-1}\right)^\gamma$$

the system (13) is correct for the whole interval  $\lambda_1 < \lambda < h$ .

Extracting the principal parts of the formulas (19) in the neighborhood of the singular points  $\lambda_1$  and  $\lambda_2 \neq 1$ , we find that in the first case  $\sqrt{K} \approx \text{const } s^{-1/3}$  and in the second case  $\sqrt{K} = \text{const } s$ , where  $s$  is to be computed respectively for  $\lambda_1$  and  $\lambda_2$ .

For  $k = 0$  we have the usual equations of Chaplygin. For separate formulas  $p = p(\rho)$  and values  $k_1$  a system of equations in Legendre functions can be found which are more convenient for solution than the system (13).

We will pass from the functions  $\phi, \psi$  to the functions  $\Phi, \Psi$  by means of the Legendre transformation

$$\Phi = x \frac{\partial \phi}{\partial x} + y \frac{\partial \phi}{\partial y} - \phi, \quad \Psi = x \frac{\partial \psi}{\partial x} + y \frac{\partial \psi}{\partial y} - \psi \quad (20)$$

We have

$$x = \Phi_{u^*} = -\Psi_t, \quad y = \Phi_{v^*} = \Psi_r, \quad \left(r = \frac{\cos \theta}{Q}, t = \frac{\sin \theta}{Q}\right) \quad (21)$$

In the independent variables  $s, \theta$  the system (21) has the following form (see, for instance, [7])

$$\frac{\partial \Psi}{\partial \theta} = -\sqrt{K_1} \frac{\partial \Phi}{\partial s}, \quad \frac{\partial \Psi}{\partial s} = \sqrt{K_1} \frac{\partial \Phi}{\partial \theta} \quad \left(\sqrt{K_1} = \sqrt{K} \left[\frac{P}{Q}\right]^n\right)$$

Approximate and exact methods of solution of the Chaplygin equations can be used for the solution of problems of a given flow of gas in a magnetic field. For the approximations one must use a closure condition. For instance, if in the order of the approximation some other function  $f(s)$  is taken instead of the rigorous dependence on  $\sqrt{K(s)}$ , after substituting the function  $f(s)$  in place of  $\sqrt{K}$  in Equation (14) we obtain an equation for determining the functions  $P(s)$  and  $Q(s)$ . We obtain the dependence of  $\rho$  on  $w$  in the parametric form  $\rho = \rho(s)$ ,  $w = w(s)$  by means of the formulas  $w^* = P^{-1}$ ,  $\rho^* = P/Q$  and the formulas (8) and (9).

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